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DESCRIPTION

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EASY-TO-TEAR STRETCHED ALIPHATIC POLYESTER FILM

Technical Field

The present invention relates to an easily tearable
5 biodegradable stretched aliphatic polyester film. Particularly,
the present invention relates to a stretched aliphatic
polyester film superior in heat resistance, biodegradability,
aroma retention, water resistance and mechanical property,
which has fine easy-to-tear property and twist fixability
10 useful for a packaging film or a film for adhesive tapes.

In addition, the present invention relates to a
stretched aliphatic polyester film having characteristics of a
cellophane film having both antinomic characteristics of
superior easy-to-tear property and superior tensile impact
15 property, wherein defects of a cellophane film in moisture
resistance and biodegradability have been improved.

Furthermore, the present invention relates to an
environment corresponding type packaging bag superior in easy-
to-cut property, which has characteristics of a stretched
20 aliphatic polyester film in heat resistance, biodegradability,
aroma retention, toughness and the like.

Background Art

Conventionally, as a film having superior easy-to-tear
property, a cellophane film has been known. Since cellophane
25 film shows fine characteristics in transparency, easy-to-tear
property, twist fixability and the like, it has been widely
used as a packaging material of food and pharmaceutical
products, a material for adhesive tapes and the like. However,
cellophane film has high hygroscopicity and the
30 characteristics of the film vary depending on the season,
which makes it difficult to always provide a film having
constant quality. In addition, since cellophane film requires
use of large amounts of highly toxic substances during the

production step thereof, such as sulfuric acid and carbon disulfide, once these flow out, a serious environmental pollution may occur.

On the other hand, packaging bags and adhesive tapes
5 comprising a polyethylene terephthalate film as a substrate are superior in toughness, heat resistance, water resistance and transparency of the film. As packaging bags, however, they are associated with defects in that the bag is difficult to open by tearing and the bag cannot be used for twist packaging
10 due to its inferior twist fixability, and as adhesive tapes, they are associated with defects in that the tape resists cutting by hand or a dispenser, and the like.

As a method for solving the above-mentioned defects, there have been proposed a monoaxially oriented polyester film
15 (JP-B-55-8551), a film wherein diethylene glycol component and the like are copolymerized (JP-B-56-50692), a film obtained from a low molecular weight polyester resin (JP-B-55-20514) and the like.

In the above-mentioned conventional techniques, however,
20 a method comprising monoaxial orientation permits easy linear cutting in the orientation direction but otherwise in the directions other than the orientation direction. In addition, a method comprising copolymerization of large amounts of diethylene glycol component and the like is defective in that
25 the copolymerization impairs toughness and heat resistance that polyethylene terephthalate originally has. Furthermore, a method using a low molecular weight polyester resin is not practical because problems such as breakage in the drawing step easily occur.

30 In JP-A-5-104618, in contrast, a film having fine tearing performance and twist fixability while maintaining characteristics such as heat resistance, aroma retention, water resistance and toughness has been obtained by employing

a multi-layer constitution of a polyester film consisting of polyester resins having different melting points and controlling the temperature of the heat treatment during the production step. Moreover, problem of breakage has been
5 reduced during the drawing step. However, even this film does not show entirely sufficient tearing performance and twist fixability. In addition, the burden on the environment has not been considered due to the absence of biodegradability.

In the meantime, a film superior in tearing-by-hand
10 performance, i.e., tearability, which is made from a polystyrene polymer having a syndiotactic structure, wherein the defects of the aforementioned cellophane film in moisture resistance and the like have been improved, is drawing attention, and, for example, JP-A-5-33809, JP-A-2000-25835,
15 JP-A-2002-240209 and the like propose various packaging bags made of a film produced using the polystyrene polymer having the syndiotactic structure.

Certainly, the film obtained by the aforementioned known method shows improved easy-to-tear property, which is one of
20 the characteristics that a cellophane film has, and is of a practical level. However, tensile impact strength, which is the other characteristic, has not been improved, and the development of the film in the field requiring impact resistance has not been attainable.

25 In view of the serious problems of waste in recent years, moreover, prevailing of packaging materials and adhesive tape materials associated with a smaller environmental burden has been desired. To be precise, when polyesters such as polyethylene terephthalate and the like are wasted by land-
30 fill in the form of a film or a sheet, they remain under natural environment and cause environmental pollution because they resist corrosion and decomposition. Even when they are incinerated, the incinerator may be undesirably damaged and

toxic gas may be undesirably generated due to the high calorific power of the materials themselves, or laminate materials and additives.

To deal with such problems, development of a
5 biodegradable material to be decomposed by microorganisms present in nature has been ongoing. Particularly, a lactic acid-based polyester film is superior in heat resistance, aroma retention, transparency, toughness and form-processability, and exploitation of use in a wide range is
10 being realized, as, for example, packaging materials, adhesive tape materials, containers, electronic parts-related materials and the like. However, due to its easy-to-tear performance, which is not superior, when this film is used as a packaging bag, the bag shows problematically inferior easy-to-cut
15 property.

Brief Description of the Drawings

Fig. 1 is a schematic view showing the shape of a sample for tear energy measurement.

20 Fig. 2 is a schematic view showing the maximum strength and the elongation at the point of the maximum strength, on the S-S curve obtained in the tear energy measurement.

Disclosure of the Invention

An object of the present invention is to provide an
25 environment corresponding type film, having easy-to-tear property, twist fixability and transparency, which are characteristics of a cellophane film, as well as heat resistance, biodegradability, aroma retention, toughness and the like, which are characteristics of a stretched aliphatic
30 polyester film, in combination.

Another object of the present invention is to provide an environment corresponding type biodegradable film having both the antinomic characteristics of a cellophane film: superior

easy-to-tear performance and superior tensile impact property, wherein moisture resistance, which is a defect of the cellophane film, has been improved.

In addition, another object of the present invention is
5 to provide an environment corresponding type packaging bag having easy-to-cut property, as well as biodegradability, heat resistance, aroma retention, toughness and the like in combination.

The present inventors have conducted intensive studies
10 in an attempt to achieve the above-mentioned objects and found that an easy-to-tear film can be obtained by, for example, irradiation of actinic rays on a stretched aliphatic polyester film, thereby setting an edge tear strength of the film in the longitudinal direction and the transverse direction to not
15 more than 22 N.

It has been also found that a film having both the antinomic characteristics of a cellophane film of superior easy-to-tear performance and superior tensile impact property can be obtained by, for example, irradiation of actinic rays
20 on a stretched aliphatic polyester film containing a flexible polyester resin to afford a film having particular tear energy and tensile impact strength.

Furthermore, as a production method of the aforementioned easy-to-tear film, a method of laminating
25 aliphatic polyesters having different melting points in three layers of A/B/A under particular film-forming conditions.

Accordingly, the present invention provides the following

(1) to (9):

(1) an easy-to-tear stretched aliphatic polyester film having
30 an edge tear strength in the longitudinal direction and the transverse direction of not more than 22 N,

(2) an easy-to-tear aliphatic polyester film having a molecular absorption coefficient at a wavelength of 205 nm of

not less than 1500,

(3) an easy-to-tear stretched aliphatic polyester film having a tear energy of 0.2-5 gf·mm/μm, and a tensile impact strength of not less than 0.5 j/mm²,

5 (4) the easy-to-tear stretched aliphatic polyester film of any one of (1) to (3), which is produced by irradiation of actinic rays on a stretched aliphatic polyester film,

(5) the easy-to-tear stretched aliphatic polyester film of any one of (1) to (4), wherein a main component of the stretched
10 aliphatic polyester film is a lactic acid-based polyester resin,

(6) an easy-to-cut packaging bag produced using a film obtained by irradiation of actinic rays on an aliphatic polyester film,

15 (7) an easy-to-cut packaging bag obtained by irradiation of actinic rays on a packaging bag produced using an aliphatic polyester film,

(8) the easy-to-tear bag of any one of (6) and (7), wherein a main component of the aliphatic polyester film is a lactic
20 acid-based polyester resin, and

(9) a production method of a lactic acid-based polyester film, which comprises stretching, in at least a monoaxial direction, a non-stretched laminate film comprising a lactic acid-based polyester resin
25 layer (A) having a melting point: T_{m_A} and a resin (B) having a melting point: T_{m_B} , which satisfies $T_{m_B} \geq T_{m_A} + 10^\circ\text{C}$, relative to T_{m_A} , said resin (B) being laminated on at least one surface of layer (A) in a thickness of 5-60% of the thickness of a whole film, and then
30 performing a heat treatment at a temperature T_s satisfying $T_{m_A} - 10^\circ\text{C} \leq T_s < T_{m_B} + 10^\circ\text{C}$.

The present invention is explained in more detail in the following.

As the aliphatic polyester resin, which is a starting material resin of the main component of the easy-to-tear stretched aliphatic polyester films of (1)-(9) of the present invention, for example, aliphatic polyester resins such as
5 polybutylene succinate, polyhydroxybutyrate, polylactic acid and the like obtained from aliphatic dicarboxylic acid and aliphatic diol, or aliphatic hydroxycarboxylic acid or aliphatic lactide can be mentioned. These aliphatic polyester resins may be copolymerized. It is also possible to mix these
10 resins with a resin compatible or incompatible with these resins. Particularly, a film comprising a lactic acid-based polyester resin as a main component is preferable, because a film that satisfies the characteristics of the present invention can be easily obtained and the film is superior in
15 heat resistance, aroma retention, transparency, toughness and form-processability.

As the aforementioned lactic acid-based polyester resin, L-lactic acid polymer, D-lactic acid polymer, a blend thereof, a copolymer thereof, a copolymer thereof with
20 polyhydroxybutyrate and the like, a mixture with other resin and the like can be mentioned.

The molecular weight of the aforementioned aliphatic polyester resin in the case of a lactic acid-based polyester resin, for example, is preferably not less than 10000 to not
25 more than 500000, particularly preferably not less than 30000 to not more than 300000, in a weight average molecular weight. When the weight average molecular weight is less than 10000, stable extrusion and casting is difficult to perform and when it exceeds 500000, melt extrusion tends to become difficult
30 due to an increased pressure in an extruder.

As long as the effect of the present invention is not inhibited, various known additives such as lubricant, pigment, thermal stabilizer, antioxidant, antistatic agent, impact

resistance improving agent and the like may be added to the easy-to-tear stretched aliphatic polyester film of the present invention.

The easy-to-tear stretched aliphatic polyester film of the present invention (1) needs to have an edge tear strength of not more than 22 N in the longitudinal direction and the transverse direction. The edge tear strength is more preferably not more than 20 N and particularly preferably not more than 18 N. When the edge tear strength exceeds 22 N, easy-to-tear property and twist fixability become unpreferably degraded. When the edge tear strength is too small, breakage may occur during a film processing step and the like, and therefore, the edge tear strength is preferably not less than 2 N.

The easy-to-tear stretched aliphatic polyester film of the present invention (2) has a molecular absorption coefficient of not less than 1500 at a wavelength of 205 nm. For this film, for example, a method comprising chemical modification of aliphatic polyester by photochemical reaction by ultraviolet irradiation of aliphatic polyester film can be mentioned. While the molecular absorption coefficient at a wavelength 205 nm of the aliphatic polyester film obtained by conventional film-forming is less than 1500, the molar molecular absorption coefficient can be increased to not less than 1500 by chemical modification, thereby allowing a film to express easy-to-tear property and twist fixability.

The easy-to-tear stretched aliphatic polyester film of the present invention (3) has a tear energy of 0.2–5 gf·mm/μm and a tensile impact strength of not less than 0.5 j/mm². Preferably, the tear energy is 0.2–4 gf·mm/μm and the tensile impact strength is not less than 0.55 j/mm². The tear energy is an index of the tearability of the film and the tensile impact strength is the strength of the film upon impact on the

film. When the tear energy is less than $0.2 \text{ gf}\cdot\text{mm}/\mu\text{m}$, the energy is too low and the film can be torn with a weak force, which is not preferable. Conversely, when it exceeds $5 \text{ gf}\cdot\text{mm}/\mu\text{m}$, the tear energy becomes too high and the tearability is degraded, which in turn unpreferably degrades, for example, tearing-by-hand performance and the like. On the other hand, when the tensile impact strength is less than $0.55 \text{ j}/\text{mm}^2$, the tensile impact strength becomes insufficient to allow breakage of film upon weak impact. Therefore, by meeting the
10 aforementioned characteristics, the antinomic characteristics of superior tearing-by-hand performance and superior impact resistance of a cellophane film can be imparted and the film can be preferably used in the field of packaging and the like.

One production method of the easy-to-tear stretched
15 aliphatic polyester films of the present invention (1)-(3) is, for example, irradiation of actinic rays on an aliphatic polyester film, as described in (4).

In another production method of the easy-to-tear stretched aliphatic polyester films of the present invention
20 (1)-(3), irradiation of actinic rays is not essential and the film is produced by, for example, laminating aliphatic polyesters having different melting points in three layers of A/B/A under particular film-forming conditions, as described in (9).

25 The production of the films of the present invention (1)-(3) by irradiation of actinic rays is explained further.

In this case, the film-forming method of the stretched aliphatic polyester film before actinic ray irradiation is not limited and may be any method. For example, an aliphatic
30 polyester resin is melted in an extruder and the like at a temperature of not less than the melting point and extruded from a die outlet to give a non-stretched film. This non-stretched film is further subjected to monoaxial stretching or

biaxial stretching and, where necessary, a heat-set treatment. Particularly, a biaxially stretched film is preferable because it shows less degree of uneven thickness and a film having a uniform tear direction can be easily obtained.

5 The stretched polyester film before actinic ray irradiation may be a single layer film or a laminate film, and when it is a laminate film, for example, a non-stretched film can be obtained by a method comprising separately melting resins in plural extruders at a temperature not less than the
10 melting point, extruding them from a die outlet and laminating the formed non-stretched films with heating, a method comprising melt-laminating a molten film on the surface of a different non-stretched film, a method comprising laminating resins in a molten state in a feed block or a die by co-
15 extrusion methods, extruding same from a die outlet and cool-solidifying the laminate and the like. The die may be either a flat die or a cyclic die.

 The obtained single-layer or multi-layer non-stretched film is subjected to monoaxial stretching or biaxial
20 stretching at a temperature not more than the melting point of the aliphatic polyester resin. In the case of a lactic acid-based polyester resin, for example, the film is stretched at 40°C-170°C. The draw ratio is at least not less than 1.5, preferably 3 to 5 for the monoaxial stretching, and not less
25 than 10, preferably not less than 16, in area ratios for the biaxial stretching. When the draw ratio is low, tearing performance and the degree of uneven thickness of the stretched film become degraded. When the draw ratio is too high, problems occur in that the directional property of
30 tearing becomes intense and incident of breakage increases during production, thus degrading productivity. In the case of biaxial stretching, moreover, any of sequential stretching methods and simultaneous stretching methods can be used. The

stretching method may be any of roll stretching methods, tenter stretching methods and inflation methods.

The stretched aliphatic polyester film of the present invention is preferably subjected to a heat treatment after stretching to impart easy-to-tear property. For example, the heat treatment is conducted at a temperature of 0-50°C lower than the melting point of the aliphatic polyester resin. In the case of a lactic acid-based polyester resin, for example, the heat treatment is preferably conducted at 130°C-170°C. When the temperature of the heat treatment is too low, the molecular orientation cannot be broken and a film having fine tearability may not be obtained. When the temperature of the heat treatment is too high, the film gets perforated and breakage occurs often, thus making the film-forming difficult. When a heat-relaxation treatment is applied after the heat-set treatment, thermal dimensional stability is improved preferably.

The easy-to-tear property and twist fixability can be improved by selecting suitable drawing conditions, heat treatment conditions and laminate thickness constitution. Such methods can be employed without any limitation.

The film of the present invention (3) can be obtained by, for example, actinic ray treatment of an aliphatic polyester film obtained in the same manner as above by adding a polyester elastomer or a flexible polyester polymer such as flexible aliphatic polyester polymer and the like to the aforementioned starting material aliphatic polyester resin in a proportion of 3-30 parts by weight relative to 100 parts by weight of the aliphatic polyester resin. It is also preferable to set the draw ratio lower for the production of the film. As the aforementioned flexible polyester polymer for modification, use of an aliphatic polyester polymer is a more preferable embodiment from the aspect of biodegradability.

To obtain an easy-to-tear stretched aliphatic polyester film, actinic rays are irradiated on the aliphatic polyester film obtained by the aforementioned method. The kind of the actinic rays is not particularly limited as long as it has energy capable of chemical modification of the structure of the aliphatic polyester. For example, ultraviolet ray, electron beam, γ -ray, X-ray and the like can be mentioned. As the source of the ultraviolet ray, one having an emission wavelength in the absorption wavelength region of the stretched aliphatic polyester film is preferable. For example, an artificial light source such as a low pressure mercury lamp, a high pressure mercury lamp, a chemical lamp, a xenon lamp, a zirconium lamp, a carbon arc lamp, a germicidal lamp and the like can be mentioned, but the source is not limited thereto. A natural light such as sunlight is not practical because its illuminance is low.

A method of the aforementioned irradiation treatment using actinic rays may be an inline treatment during film-forming or a batch treatment after film-forming, or further, the treatment may be applied after processing into a packaging bag and the like, wherein the method is not limited.

The easy-to-tear stretched aliphatic polyester films of the present invention (1)-(3) may be subjected to surface processing to improve adhesiveness, printability and the like by a known coating method, during a film-forming step. In addition, surface processing such as a corona treatment, a plasma treatment, a flame treatment and the like may be applied to improve the wettability and adhesiveness of the surface of the aliphatic polyester film.

The easy-to-tear stretched aliphatic polyester films of the present invention (1)-(3) as packaging materials can be made to have heat seal property by laminating a resin layer having heat seal property by known methods such as dry

lamination, extrusion lamination and the like. In this case, various biodegradable resin layers are preferably laminated from the viewpoint of biodegradability.

The films of the present invention (1)-(3) can be
5 preferably used as easy-to-cut packaging bags.

The present invention (6) and (7) relates to an easy-to-cut packaging bag. The present invention (6) is an easy-to-cut packaging bag produced from a film obtained by irradiation of actinic rays on an aliphatic polyester film, and the present
10 invention (7) is an easy-to-cut packaging bag obtained by irradiation of actinic rays on a packaging bag produced using an aliphatic polyester film.

The sealing method of the easy-to-cut packaging bags of the present invention (6) and (7) is not limited and may be
15 any, but a heat sealing method can be mentioned as a preferable method. When the heat sealing method is practiced, a method comprising laminating the aforementioned aliphatic polyester film on a resin layer having heat seal property and imparting the heat seal property thereto is a preferable
20 embodiment. While the lamination method is not limited, known methods such as dry lamination, extrusion lamination and the like are preferably employed. In these methods, the kind of resin layer having heat seal property is not limited; but the layer preferably consists of a degradable resin. Particularly
25 from the viewpoint of biodegradability, lamination of various biodegradable resin layers is most preferable. In other words, it is preferable to use a film made from a resin having a melting point or softening point lower than that of the aforementioned aliphatic polyester film. The use of a non-
30 stretched film is particularly preferable.

The bag-making method is not limited and may be any, and, for example, a packaging bag manufactured by a three-side-sealed bag forming machine or a center sealed bag forming

machine can be mentioned. In addition, it may be a packaging bag produced simultaneously with filling using an automatic filling machine.

The packaging bags obtained by the present invention (6) and (7) have easy-to-cut property and an auxiliary means to impart the easy-to-cut property is not necessarily required. Depending on the demand in the market, however, a notch may be formed, or perforation and the like may be performed without restriction, thereby to form an auxiliary means to improve tearing-by-hand performance.

In the present invention (7), the actinic ray treatment to impart easy-to-cut property is applied to a produced packaging bag. Therefore, the aliphatic polyester film can go through the film-forming step and the bag making step prior to this treatment, in the state of a tough film before imparting the easy-to-cut property. As a result, these steps can be characteristically performed without lowering the operability.

Now, the case where the films of the present invention (1)-(3) are produced without irradiation of actinic rays, or a method of producing a film of the present invention (9), wherein aliphatic polyesters having different melting points are laminated in three layers of A/B/A under particular film-forming conditions is explained.

The aforementioned lactic acid-based polyester can be used for the lactic acid-based polyester resin layer (A) and (B) of the present invention (9). Here, the polyester used for lactic acid-based polyester resin layer (A) has a melting point of not less than 10°C lower, preferably not less than 20°C lower, than the melting point of the polyester used for the lactic acid-based polyester resin layer (B). As a method of controlling the melting points of the lactic acid-based polyester resin layer (A) and (B), for example, a method comprising changing the D-lactic acid ratio of the lactic acid

polymer, a method comprising changing the hydroxycarboxylic acid component ratio and the like can be mentioned.

The weight average molecular weight of the polyester of the lactic acid-based polyester resin layers (A) and (B) is each preferably not less than 50000 and not more than 500000, particularly preferably not less than 80000 and not more than 300000. When the weight average molecular weight is less than 50000, film-forming tends to become unstable when a starting material is melt-extruded and performing casting, and when it exceeds 500000, melt extrusion tends to be difficult due to the increased pressure in an extruder.

The polyester of the lactic acid-based polyester resin layers (A) and (B) of the present invention may contain various known additives such as lubricant, pigment, thermal stabilizer, antioxidant, antistatic agent, impact resistance improving agent and the like, as long as the effect of the present invention is not inhibited.

The thickness of the lactic acid-based polyester resin layer (B) is not less than 5%, not more than 60%, and preferably 15% to 50%, of the thickness of the entire film. When the thickness of the lactic acid-based polyester resin layer (B) is less than 5% of the thickness of the entire film, the strength of the obtained film becomes insufficient, causing practical inconvenience. When the thickness of the lactic acid-based polyester resin layer (B) exceeds 60% of the entire thickness, sufficient tearability and twist property cannot be achieved unpreferably. The constitution of the lactic acid-based polyester resin layer (A) and the lactic acid-based polyester resin layer (B) may be a three-layer (B/A/B, A/B/A) or two-layer (B/A) construction. While the thickness of the stretched film is not particularly limited, 12 μm - 30 μm is preferable for use as a packaging bag, an adhesive tape and the like.

The production method of the non-stretched laminate film in the present invention (9) may be any of the following. (1) a method comprising separately melting resins in plural extruders and the like at a temperature not less than the melting point, extruding them from a die outlet and laminating the formed non-stretched films with heating, (2) a method comprising melt-laminating a molten film on the surface of a different non-stretched film, (3) a method according to a co-extrusion method, which comprises laminating resins in a molten state in a feed block or a die, extruding same from a die outlet and cool-solidifying the laminate and the like.

The extrusion temperature is preferably in the range of $T_{mB} - (T_{mB} + 70^{\circ}\text{C})$, particularly preferably in the range of $(T_{mB} + 20^{\circ}\text{C}) - (T_{mB} + 50^{\circ}\text{C})$, relative to the melting point: T_{mB} of polyester (B) having higher melting point. When the extrusion temperature is less than T_{mB} , the extrusion tends to be difficult due to the increased pressure in an extruder. In contrast, when it exceeds $(T_{mB} + 70^{\circ}\text{C})$, thermal decomposition of the lactic acid-based polyester resin unpreferably proceeds. The die of the extruder used in the present invention may be cyclic or may have a linear slit.

The thus-obtained non-stretched laminate film is subjected to monoaxial stretching or biaxial stretching at a temperature which is higher than the higher of the glass transition points of the lactic acid-based polyester resin (A) and the lactic acid-based polyester resin (B), and not higher than the melting point T_{mA} of the polyester resin (A). The draw ratio in the case of monoaxial stretching is at least not less than 1.5, preferably 3 to 7, and in the case of biaxial stretching, 1.5 to 10 in each direction and not less than 10, preferably not less than 16, in area ratio. In the case of biaxial stretching, any of sequential biaxially stretching methods and simultaneous biaxially stretching methods may be

used.

As the stretching machine in the present invention, for example, an inflation film-forming machine, a roll stretching machine, a tenter stretching machine (transversely stretching type, pantographic simultaneous biaxially stretching type, linear motor driven simultaneous biaxially stretching type) and the like can be mentioned.

In the present invention, it is important that a heat treatment should be applied to a stretched film at a temperature T_s satisfying $T_{m_A}-10^{\circ}\text{C}\leq T_s<T_{m_B}+10^{\circ}\text{C}$, more preferably a temperature satisfying $T_{m_A}\leq T_s<T_{m_B}$, for 2 seconds to 30 seconds, more preferably 5 seconds to 15 seconds. While the heat treatment can be applied at a fixed width, it can be also applied with relaxation or under tension. When the temperature of the heat treatment is $T_s<T_{m_A}-10^{\circ}\text{C}$, the molecular orientation of the lactic acid-based polyester resin layer (A) cannot be broken, and fine tearability and fine twist fixability cannot be obtained. When the temperature of the heat treatment is $T_s>T_{m_B}+10^{\circ}\text{C}$, the film may have holes, or film itself may be melted to make the film-forming difficult. In other words, heat treatment operation at a suitable temperature and control of the thickness of the constitution enable balancing between a layer having disintegrated molecular orientation that affords tearability and twist property, and a layer maintaining molecular orientation that affords heat resistance and toughness that are the characteristics a stretched lactic acid-based polyester film originally has, whereby the conflicting properties can be simultaneously maintained.

In the present invention (9), therefore, a non-stretched laminate film comprising lactic acid-based polyester layers (A) and (B) having different melting points is stretched in at least one direction and a heat treatment is applied at a temperature not lower than 10°C lower than the melting point:

measured from room temperature to 220°C at a temperature rise rate of 10°C/min and the peak temperature was taken as the melting point.

(2) Weight average molecular weight

5 A solution of polystyrene (manufactured by TOSOH CORPORATION) was prepared as a standard substance and a GPC calibration curve was plotted. For the measurement by RI detection, GPC (Shodex-System-21 manufactured by SHOWA DENKO K.K.) was used, columns (GMH×1, GMH×1, G2000H×1 (manufactured
10 by TOSOH CORPORATION) were serially connected and used, as a developing solvent, chloroform was used at a column temperature of 40°C. The data was processed using SIC-480, manufactured by System Instruments CO., LTD., to calculate the weight average molecular weight.

15 (3) Molecular absorption coefficient

 The molecular absorption coefficient is a coefficient specific to a substance, as described in Physical and Chemical Dictionary (Iwanami Shoten, 3rd ed. enlarged ed. page 1350, molar absorption coefficient). The ultraviolet absorption
20 spectrum of the film having a thickness of about 5 μm, which was cast by the following method, was measured by recording spectrophotometer U-3500 (manufactured by Hitachi, Ltd.) and the coefficient was calculated from absorbance A at wavelength 205 nm by Lambert-Beer formula (measurement condition: scan
25 speed; 60 mm/min, sampling interval; 0.1 nm).

Molecular absorption coefficient $\epsilon = A/b \cdot c$

A: absorbance (-), b: film thickness (cm), c: molar concentration was 1.

 Casting method of measurement film: A sample was
30 dissolved in chloroform at a concentration of 10% and the obtained solution was dropped on a fluorine resin-treated surface of a substrate comprising a fluorine resin-treated aluminum foil laminated on a glass plate, applied with a 50 μm

gap squeegee and dried at room temperature for 10 min. The dried film was peeled off and vacuum dried at 50°C for 2 hr to give a measurement film.

(4) Edge tear strength

5 Measured in accordance with JIS C2318-1975. A smaller value means easier tearing.

(5) Easy-to-tear property

A functional evaluation was performed. A 15 mm wide sample tape was cut out in both the longitudinal and
10 transverse directions and the sample in each direction was torn by hand. A tape that was torn easily was evaluated as ⊙, a tape that was torn easily, though in a somewhat inferior manner, was evaluated as ●, a tape that was not torn easily was evaluated as △ and a tape that could not be torn by hand
15 was evaluated as ×.

(6) Twist fixability

A functional evaluation was performed. A 30 mm wide sample tape was twisted by hand, and a tape that kept the twisted state and failed to restore to the original state was
20 evaluated as ● and a tape that failed to maintain the twisted state was evaluated as ×.

(7) Tear energy

A sample having a size of 100 mm×50 mm was cut out in such a manner that the longitudinal direction of the film and
25 the longitudinal direction of the sample matched. A 50 mm long notch was created at the center of the sample on a minor axis side in parallel with the longitudinal direction from an end. At the end point of this notch, a 4 mm diameter hole about the notch was made with a punch. The shape of this sample is shown
30 in Fig. 1. Using said sample, a tear test was performed in accordance with Trouser method, JIS-K7128. The maximum strength (gf) and the elongation (mm) showing the maximum strength were determined from the obtained S-S curve, and the

product of the two divided by the film thickness (μm) was taken as a tear energy. A schematic view of the S-S curve obtained by this measurement is shown in Fig. 2. The measurement was conducted seven times, and the tear energy was expressed with an average value of five measured values excluding the maximum value and the minimum value.

The tear test was performed under the following conditions.

Measurement apparatus: Autograph AG5000A manufactured by
10 SHIMADZU CORPORATION

Tension speed: 200 mm/min

Chart speed: 200 mm/min

(8) Tensile impact strength

A sample having a size of 100 mm in the longitudinal
15 direction and 10 mm in the transverse direction was cut out from a film to prepare a measurement sample. The measurement was conducted using UNIVERSAL IMPACT TESTER manufactured by Toyo Seiki Seisaku-sho, LTD. and according to the following method. One of the measurement samples was set on a cross head
20 and the other on a hammer, and the arm was shaken down from a lifting angle 135 (degrees) (full scale of swing at the air: 10 kgf). The angle of the position where a pointer stopped was read. From this angle and the following formula, tensile impact strength (K) was calculated. The measurement was
25 conducted eight times for each sample, and the tensile impact strength was expressed with an average value of six measured values excluding the maximum value and the minimum value.

$$K = E \times 9.807 \times 10^{-2} / (T \times W)$$

K; tensile impact strength (J/mm^2)

30 $E = 0.7071 \times WR + WR \cos \beta$

T; sample thickness (mm)

W; sample width (mm)

E; work ($\text{kgf} \times \text{cm}$)

WR; 5.8579 (kgf×cm)

β ; measured angle (degrees)

(9) Easy-to-cut property of packaging bag

A functional evaluation was performed. A packaging bag
5 produced by heat sealing by three-side sealing method was cut
by hand in the longitudinal and the transverse directions from
the sealed part. A bag that was torn easily by hand was
evaluated as ⊙, a bag that was torn easily, though in a
somewhat inferior manner, was evaluated as ●, a bag that was
10 not torn easily by hand was evaluated as Δ and a bag that
could not be torn by hand was evaluated as X.

(Example (1)-1)

An L-lactic acid-based copolymer having a melting point
15 of 175°C and a weight average molecular weight of 170000 was
melted in a twin-screw extruder (screw diameter =35φ, L/D=45:
TEM manufactured by TOSHIBA MACHINE CO., LTD.) and extruded
from a T-die at 200°C to give a non-stretched film.

This non-stretched film was first stretched 3.4 times in
20 the longitudinal direction at 75°C by a roll stretching machine
and then 5.5 times in the transverse direction at 85°C by a
tenter stretching machine, after which it was subjected to a
heat-set treatment at 155°C and a 3% relaxation treatment in
temperature descending process, whereby a 25 μm film was
25 obtained. This film-forming was free of any problem such as
breakage and the productivity was fine.

This film was subjected to an ultraviolet irradiation
treatment for 3 min. using an ultraviolet irradiation
treatment apparatus with a germicide lamp (germicide lamp
30 GL20-A manufactured by TOSHIBA CORPORATION) attached to an
exposure machine (JEA2SS manufactured by NIHON DENSHI SEIKI
CO., LTD.). The film after the ultraviolet irradiation
treatment was subjected to a functional test for easy-to-tear

property and twist fixability. The film after the ultraviolet irradiation treatment showed fine easy-to-tear property in every direction. In addition, twist fixability was fine.

5

(Example (1)-2)

By the same method as used in Example (1)-1 except that the ultraviolet irradiation treatment was applied for 10 min., a stretched film was obtained, and then an ultraviolet
10 irradiation-treated film was obtained. The film after the ultraviolet irradiation treatment showed fine easy-to-tear performance in any direction. In addition, twist fixability was fine.

(Example (1)-3)

15 By the same method as used in Example (1)-1 except that the ultraviolet irradiation treatment was applied for 20 min., a stretched film was obtained, and then an ultraviolet irradiation-treated film was obtained. The film after the ultraviolet irradiation treatment showed fine easy-to-tear
20 performance in any direction. In addition, twist fixability was fine.

(Examples (1)-4 and (1)-5)

In the method of Example (1)-1, stretched aliphatic polyester films obtained by the same method as used in Example
25 (1)-1 were introduced into an electron beam irradiation device without ultraviolet irradiation, and an electron beam (15 and 20 Mrad energy, respectively) was irradiated at 200 KV, whereby easy-to-tear stretched aliphatic polyester films of Examples (1)-4 and (1)-5 were obtained. The films obtained in
30 these Examples showed easy-to-tear performance in any direction. In addition, twist fixability was fine.

(Comparative Example (1)-1)

The film prior to the ultraviolet irradiation treatment

in Example (1)-1 was subjected to a functional test for easy-to-tear property and twist fixability. Tearing in the transverse direction was more difficult than a cellophane film, and cutting in the longitudinal direction was not attainable. When the film was twisted, the twisted state could not be maintained.

The evaluation results of the films obtained in Examples and Comparative Example are shown in Table 1.

10

Table 1

		Ex. (1)-1	Ex. (1)-2	Ex. (1)-3	Ex. (1)-4	Ex. (1)-5	Comp. Ex. (1)-1
film thickness	μm	25	25	25	25	25	25
melting point	°C	175	175	175	175	175	175
heat treatment temperature	°C	155	155	155	155	155	155
UV irradiation time	min.	3	10	20	—	—	untreated
electron beam irradiation energy	Mrad	—	—	—	15	20	untreated
edge tear strength	N	15	10	5	13	7	55
easy-to-tear property (transverse)	—	○	⊙	⊙	○	⊙	Δ
easy-to-tear property (longitudinal)	—	○	⊙	⊙	○	⊙	x
twist fixability	—	○	⊙	⊙	○	⊙	x

(Example (2)-1)

An L-lactic acid-based copolymer having a melting point of 175°C and a weight average molecular weight of 170000 was melted in a twin-screw extruder (screw diameter =35φ, L/D=45: 5 TEM manufactured by TOSHIBA MACHINE CO., LTD.) and extruded from a T-die at 200°C to give a non-stretched film.

This non-stretched laminate film was first stretched 3.4 times in the longitudinal direction at 75°C by a roll stretching machine and then 5.5 times in the transverse 10 direction at 85°C by a tenter stretching machine, after which it was subjected to a heat-set treatment at 155°C and a 3% relaxation treatment in a temperature descending process, whereby a 25 μm film was obtained. This film-forming was free of any problem such as breakage and the productivity was fine.

15 This film was subjected to an ultraviolet irradiation treatment for 5 min using an ultraviolet irradiation treatment apparatus with a germicide lamp (germicide lamp GL20-A manufactured by TOSHIBA CORPORATION) attached to an exposure machine (JEA2SS manufactured by NIHON DENSHI SEIKI 20 CO., LTD.). The film after the ultraviolet irradiation treatment was subjected to a functional test for easy-to-tear property and twist fixability. The film after the ultraviolet irradiation treatment showed fine easy-to-tear property in any direction. In addition, twist fixability was 25 fine.

(Example (2)-2)

By the same method as used in Example (2)-1 except that the ultraviolet irradiation treatment was applied for 10 min., a stretched film was obtained, and then an ultraviolet 30 irradiation-treated film was obtained. The film after the ultraviolet irradiation treatment showed fine easy-to-tear performance in any direction. In addition, twist fixability was fine.

(Example (2)-3)

By the same method as used in Example (2)-1 except that the ultraviolet irradiation treatment was applied for 20 min., a stretched film was obtained, and then an ultraviolet
5 irradiation-treated film was obtained. The film after the ultraviolet irradiation treatment showed fine easy-to-tear performance in any direction. In addition, twist fixability was fine.

(Comparative Example (2)-1)

10 The film prior to the ultraviolet irradiation treatment in Example (2)-1 was subjected to a functional test for easy-to-tear property and twist fixability. Tearing in the transverse direction was more difficult than a cellophane film, and cutting in the longitudinal direction was not
15 attainable. When the film was twisted, the twisted state could not be maintained.

The evaluation results of the films obtained in the Examples and the Comparative Example are shown in Table 2.

Table 2

		Ex. (2)-1	Ex. (2)-2	Ex. (2)-3	Comp. Ex. (2)-1
film thickness	μm	25	25	25	25
melting point	°C	175	175	175	175
heat treatment temperature	°C	155	155	155	155
UV irradiation time	min.	5	10	20	untreated
molecular absorption coefficient at 205 nm	-	1650	1850	2050	1450
edge tear strength	N	15	10	5	55
easy-to-tear property (transverse)	-	○	⊙	⊙	Δ
easy-to-tear property (longitudinal)	-	○	⊙	⊙	x
twist fixability	-	○	⊙	⊙	x

(Example (3)-1)

A blend comprising a copolymerized polyester polymer of succinic acid/butanediol/polycaprolactone in a proportion of 15 parts by weight relative to 100 parts by weight of an L-lactic acid-based copolymer having a melting point of 175°C and a weight average molecular weight of 170000 was melted in a twin-screw extruder (screw diameter =35φ, L/D=45: TEM manufactured by TOSHIBA MACHINE CO., LTD.) and extruded from a

T-die at 200°C to give a non-stretched film. This non-stretched film was first stretched 3.0 times in the longitudinal direction at 75°C by a roll stretching machine and then 5.0 times in the transverse direction at 85°C by a tenter stretching machine, after which it was subjected to a heat-set treatment at 155°C and a 3% relaxation treatment in a temperature descending process, whereby a 25 μm film was obtained. This film-forming was free of any problem such as breakage and the productivity was fine.

10 This film was subjected to an ultraviolet irradiation treatment for 3 min using an ultraviolet irradiation treatment apparatus with a germicide lamp (germicide lamp GL20-A manufactured by TOSHIBA CORPORATION) attached to an exposure machine (JEA2SS manufactured by NIHON DENSHI SEIKI CO., LTD.)
15 to give the easy-to-tear stretched aliphatic polyester film of Example 1. The characteristics of the obtained film are shown in Table 3.

(Example (3)-2)

20 An easy-to-tear stretched aliphatic polyester film of Example 2 was obtained by a method similar to that in Example (3)-1 except that, in the method of Example (3)-1, 10 parts by weight of a copolymerized polyester polymer comprising succinic acid/butanediol/polycaprolactone was added relative to 100 parts by weight of the L-lactic acid-based copolymer.
25 The evaluation results of the obtained film are shown in Table 3.

(Examples (3)-3 and (3)-4)

30 Easy-to-tear stretched aliphatic polyester films of Example (3)-3 and (3)-4 were obtained by a method similar to that in Example (3)-1 except that, in the method of Example (3)-1, the time of ultraviolet irradiation was set to 10 min. and 20 min., respectively. The evaluation results of the obtained films are shown in Table 3.

(Examples (3)-5 and (3)-6)

In the method of Example (3)-1, the stretched aliphatic polyester films obtained by the same method as used in Example (3)-1 were introduced into an electron beam irradiation device without ultraviolet irradiation, and an electron beam (15 and 20 Mrad, respectively) was irradiated at 200 KV, whereby the easy-to-tear stretched aliphatic polyester films of Examples (3)-5 and (3)-6 were obtained. The evaluation results of the obtained films are shown in Table 3.

10 (Comparative Example (3)-1)

In the method of Example (3)-1, the stretched aliphatic polyester film of Comparative Example 1 was obtained by a method similar to that in Example (3)-1 except that a copolymerized polyester polymer comprising succinic acid/butanediol/polycaprolactone was not added. The evaluation results of the obtained film are shown in Table 3.

(Comparative Example (3)-2)

In the method of Example (3)-1, the stretched aliphatic polyester film of Comparative Example (3)-2 was obtained by a method similar to that in Example (3)-1 except that the ultraviolet irradiation treatment was not applied. The evaluation results of the obtained film are shown in Table 3.

Table 3

	Amount of elastomer added (parts by weight)	Kind and irradiation amount of actinic rays	Tear energy (gf·mm/μm)	Tear impact strength (j/mm ²)
Example (3)-1	15	ultraviolet ray 3 min.	2.5	1.2
Example (3)-2	10	ultraviolet ray 3 min.	2.0	0.9
Example (3)-3	15	ultraviolet ray 10 min.	2.0	1.1
Example (3)-4	15	ultraviolet ray 20 min.	1.5	1.0
Example (3)-5	15	electron beam 15 Mrad	2.5	1.3
Example (3)-6	15	electron beam 20 Mrad	2.0	1.2
Comparative Example (3)-1	0	ultraviolet ray 3 min.	2.0	0.3
Comparative Example (3)-2	15	no irradiation	7.0	1.8

(Example (4)-1)

An L-lactic acid-based copolymer having a melting point of 175°C and a weight average molecular weight of 170000 was melted in a twin-screw extruder (screw diameter =35 mmφ, L/D=45: TEM manufactured by TOSHIBA MACHINE CO., LTD.) and extruded from a T-die at 200°C to give a non-stretched film.

The non-stretched film was first stretched 3.4 times in the longitudinal direction at 75°C by a roll stretching machine and then 5.5 times in the transverse direction at 85°C by a tenter stretching machine, after which it was subjected to a

heat-set treatment at 155°C and a 3% relaxation treatment in a temperature descending process, whereby a 25 µm substrate film was obtained.

On the other hand, a blend of polycaprolactone (10 parts
5 by weight) added to an L-lactic acid-based copolymer (100 parts by weight) having a melting point of 150°C and a weight average molecular weight of 150000 was extruded under the same conditions as mentioned above, and extrusion-laminated on the substrate film obtained by the aforementioned method to a
10 thickness of 50 µm to form a heat seal layer of an aliphatic polyester resin. The obtained laminate was introduced into a three-side sealing machine to prepare a three-side-sealed packaging bag.

The packaging bag obtained by the above-mentioned method
15 was introduced into an electron beam irradiation device, and an electron beam (15 Mrad) was irradiated at an accelerating voltage of 350 KV, whereby an easy-to-cut packaging bag was obtained. The easy-to-cut property evaluation results of the obtained packaging bag are shown in Table 4. The packaging bag
20 obtained in this Example was superior in easy-to-cut property. In addition, the bag showed biodegradability, was of an environment corresponding type, and was highly practical as a packaging bag.

(Examples (4)-2 and (4)-3)

25 Easy-to-cut packaging bags of Examples (4)-2 and (4)-3 were obtained by a method similar to that in Example (4)-1 except that, in Example (4)-1, the irradiation energy of electron beam irradiation was 10 and 20 Mrad, respectively. The easy-to-cut property evaluation results of the obtained
30 packaging bags are shown in Table 4. The packaging bags obtained in these Examples showed high practicality as did the packaging bag obtained in Example (4)-1.

(Example (4)-4)

An easy-to-cut packaging bag of Example (4)-4 was obtained by a method similar to that in Example 1 except that, in Example (4)-1, the electron beam irradiation was not applied and an ultraviolet irradiation treatment was applied instead for 3 min using an ultraviolet irradiation treatment apparatus with a germicide lamp (germicide lamp GL20-A, manufactured by TOSHIBA CORPORATION) attached to an exposure machine (JEA2SS manufactured by NIHON DENSHI SEIKI CO., LTD.). The easy-to-cut property evaluation results of the obtained packaging bag are shown in Table 4. The packaging bag obtained in this Example showed high practicality as did the packaging bag obtained in Example (4)-1.

(Examples (4)-5 and (4)-6)

Easy-to-cut packaging bags of Examples (4)-5 and (4)-6 were obtained by a method similar to that in Example (4)-4 except that, in Example (4)-4, the time of the ultraviolet irradiation treatment was 10 and 20 min., respectively. The easy-to-cut property evaluation results of the obtained packaging bags are shown in Table 4. The packaging bags obtained in these Examples showed high practicality as did the packaging bag obtained in Example (4)-4.

(Comparative Example (4)-1)

A packaging bag of Comparative Example (4)-1 was obtained by a method similar to that in Example (4)-1 except that, in Example (4)-1, the electron beam irradiation was not applied. The easy-to-cut property evaluation results of the obtained packaging bag are shown in Table 4. The packaging bag obtained in this Comparative Example is superior in that it has biodegradability and is of an environment corresponding type, but it has poor easy-to-cut property and of little practical use as a packaging bag requiring tearing-by-hand performance.

Table 4

	electron beam irradiation energy (Mrad)	UV irradiation time (min.)	easy-to-cut property
Example (4)-1	15	—	⊙
Example (4)-2	10	—	○
Example (4)-3	20	—	⊙
Example (4)-4	—	3	○
Example (4)-5	—	10	⊙
Example (4)-6	—	20	⊙
Comparative Example (4)-1	—	—	×

(Example (5)-1)

An L-lactic acid-based copolymer having a melting point
 5 of 175°C and a weight average molecular weight of 170000 was
 melted in a twin-screw extruder (screw diameter =35 mmφ,
 L/D=45: TEM manufactured by TOSHIBA MACHINE CO., LTD.) and
 extruded from a T-die at 200°C to give a non-stretched film.

The non-stretched film was first stretched 3.4 times in
 10 the longitudinal direction at 75°C by a roll stretching machine
 and then 5.5 times in the transverse direction at 85°C by a
 tenter stretching machine, after which it was subjected to a
 heat-set treatment at 155°C and a 3% relaxation treatment in a
 temperature descending process, whereby a 25 μm substrate film
 15 was obtained.

On the other hand, a blend of polycaprolactone (10 parts
 by weight) added to an L-lactic acid-based copolymer (100
 parts by weight) having a melting point of 150°C and a weight
 average molecular weight of 150000 was extruded under the same
 20 conditions as mentioned above, and extrusion-laminated on the
 substrate film obtained by the aforementioned method to a
 thickness of 50 μm to form a heat seal layer of an aliphatic

polyester resin.

The laminate obtained by the above-mentioned method was introduced into an electron beam irradiation device, and an electron beam (15 Mrad) was irradiated at an accelerating voltage of 350 KV. The electron beam-irradiated laminate produced by said method was introduced into a three-side sealing machine to prepare a three-side-sealed packaging bag. The easy-to-cut property evaluation results of the obtained packaging bag are shown in Table 5. The packaging bag obtained in this Example was superior in easy-to-cut property. In addition, the bag showed biodegradability, was of an environment corresponding type, and was highly practical as a packaging bag.

(Examples (5)-2 and (5)-3)

Easy-to-cut packaging bags of Examples (5)-2 and (5)-3 were obtained by a method similar to that in Example (5)-1 except that, in Example (5)-1, the irradiation energy of electron beam irradiation was 10 and 20 Mrad, respectively. The easy-to-cut property evaluation results of the obtained packaging bags are shown in Table 5. The packaging bags obtained in these Examples showed high practicality as did the packaging bag obtained in Example (5)-1.

(Example (5)-4)

An easy-to-cut packaging bag of Example (5)-4 was obtained by a method similar to that in Example 1 except that, in Example (5)-1, the electron beam irradiation was not applied and an ultraviolet irradiation treatment was applied instead for 3 min using an ultraviolet irradiation treatment apparatus with a germicide lamp (germicide lamp GL20-A, manufactured by TOSHIBA CORPORATION) attached to an exposure machine (JEA2SS manufactured by NIHON DENSHI SEIKI CO., LTD.). The easy-to-cut property evaluation results of the obtained packaging bag are shown in Table 5. The packaging bag obtained

in this Example showed high practicality as did the packaging bag obtained in Example (5)-1.

(Examples (5)-5 and (5)-6)

Easy-to-cut packaging bags of Examples (5)-5 and (5)-6 were obtained by a method similar to that in Example (5)-4 except that, in Example (5)-4, the time of the ultraviolet irradiation treatment was 10 and 20 min., respectively. The easy-to-cut property evaluation results of the obtained packaging bags are shown in Table 5. The packaging bags obtained in these Examples showed high practicality as did the packaging bag obtained in Example (5)-4.

(Comparative Example (5)-1)

A packaging bag of Comparative Example (5)-1 was obtained by a method similar to that in Example (5)-1 except that, in Example (5)-1, the electron beam irradiation was not applied. The easy-to-cut property evaluation results of the obtained packaging bag are shown in Table 5. The packaging bag obtained in this Comparative Example is superior in that it has biodegradability and is of an environment corresponding type, but it has poor easy-to-cut property and of little practical use as a packaging bag requiring easy-to-cut performance.

Table 5

	electron beam irradiation energy (Mrad)	UV irradiation time (min.)	easy-to-cut property
Example 1	15	—	⊙
Example 2	10	—	○
Example 3	20	—	⊙
Example 4	—	3	○
Example 5	—	10	⊙
Example 6	—	20	⊙
Comparative Example 1	—	—	x

(Example (6)-1)

As a starting material for lactic acid-based polyester resin layer (A), an L-lactic acid-based copolymer having a melting point of 145°C and a D-lactic acid ratio of 10% was used, and as a starting material for lactic acid-based polyester resin layer (B), an L-lactic acid-based copolymer having a melting point of 175°C and a D-lactic acid ratio of 1% was used. Both starting materials were melt-extruded using two different extruders, joined in a feed block, extruded from a T-die at 200°C and rapidly cooled by a cooling drum to give a non-stretched laminate film having a (B/A/B) constitution and a thickness of 400 μm .

This non-stretched laminate film was first stretched 3.4 times in the longitudinal direction at 75°C and then 5.5 times in the transverse direction at 85°C, after which it was subjected to a heat treatment at 155°C and a 3% relaxation treatment in a temperature descending process, whereby a 25 μm film was obtained. The thickness constitution ratio of respective layers of B/A/B of this film was 2/21/2.

The film obtained by the above film-forming step was easily cut in any direction in a functional test, and when the film was twisted, the twisted state was maintained. This film was free of any problem such as breakage during film-forming and slitting, and the productivity was fine.

(Example (6)-2)

A 25 μm film having a thickness constitution ratio of respective layers of B/A/B changed to 4/17/4 was obtained using the same starting materials and method as in Example (6)-1. This film showed a slightly resisting tearing-by-hand performance as compared to Example (6)-1 but twist fixability was fine.

(Comparative Example (6)-1)

Using the same starting materials and method as in

Example (6)-1, a 25 μm film, wherein a thickness constitution ratio of respective layers of B/A/B was changed to 10/5/10, was obtained. The thus-obtained film did not have fine tearability and restored the original state in a twist test, thus failing to achieve twist fixability.

(Comparative Example (6)-2)

A 25 μm film was obtained using the same starting materials and method as in Example (6)-1 except that the temperature of the heat treatment alone was changed to 130°C. The thus-obtained film did not have fine tearability and restored the original state in a twist test, thus failing to achieve twist fixability.

(Comparative Example (6)-3)

Using the same method, conditions and thickness ratio as in Example (6)-1 except that an L-lactic acid-based copolymer having a melting point of 169°C and a D-lactic acid ratio of 1.2% was used as a starting material for lactic acid-based polyester resin layer (A), a 25 μm film was obtained. This film did not have easy-to-tear property and restored the original state in a twist test, thus failing to achieve twist fixability.

The evaluation results of the films obtained in Examples (6)-1, (6)-2 and Comparative Examples (6)-1 to (6)-3 are shown in Table 6.

Table 6

		Ex. (6)-1	Ex. (6)-2	Comp. Ex. (6)-1	Comp. Ex. (6)-2	Comp. Ex. (6)-3
film thickness	μm	25	25	25	25	25
layer A thickness	μm	21	17	5	21	5
layer B ratio	%	16	32	80	16	80
layer A resin melting point	°C	145	145	145	145	169
layer B resin melting point	°C	175	175	175	175	175
heat treatment temperature	°C	155	155	155	130	155
edge tear strength	N	5	10	34	31	55
easy-to-tear property	-	⊙	○	×	×	×
twist fixability	-	○	○	×	×	×

Industrial Applicability

5

The stretched aliphatic polyester film obtained by the present invention is an environment corresponding type biodegradable film having easy-to-tear property, twist fixability and transparency, that are the characteristics of a cellophane film, as well as heat resistance, aroma retention and toughness, that an aliphatic polyester film has, in combination. Therefore, it is preferable as a packaging material for food, pharmaceutical products, electronic parts

and the like, or a material of adhesive tapes.

In addition, the stretched aliphatic polyester film obtained by the present invention (3) has the characteristics of a cellophane film having both antinomic characteristics of
5 superior easy-to-tear property and superior tensile impact property, and therefore, it is preferable as a packaging material of food, pharmaceutical products, electronic parts and the like, or a material of adhesive tapes.

Moreover, since a packaging bag made of the aliphatic
10 polyester film of the present invention (6) or (7) is superior in easy-to-cut property and is an environment corresponding type biodegradable film having heat resistance, aroma retention and toughness, that an aliphatic polyester film has, in combination, it is preferable as a packaging bag for food,
15 pharmaceutical products, electronic parts and the like.